# Development of 3D Printable Composite Inks for Millimeter Wave Applications

Bradley Duncan, Maxwell Plaut, Benjamin Barclay, John Russo, and Theodore Fedynyshyn Chemical, Microsystem, and Nanoscale Technologies Group MIT Lincoln Laboratory Lexington, MA, USA

bradley.duncan@ll.mit.edu, maxwell.plaut@ll.mit.edu, benjamin.barclay@ll.mit.edu, jar@ll.mit.edu, fedynyshyn@ll.mit.edu

Abstract— This paper presents the development of a series of conductive and dielectric inks for 3D printing. The dielectric inks were found to possess dielectric constants ranging from 2-26.5 with loss tangents on the order of  $10^{-4}-10^{-2}$  over the 26.5 to 40 GHz range ( $K_a$  band). The fabrication of gradient dielectrics via a custom active mixing nozzle is also described.

Keywords—3D printing; composites; gradient dielectrics; conductive traces; millimeter wave

## I. INTRODUCTION

3D printing of RF devices offers a powerful strategy to generate structures not achievable through typical fabrication methods [1]. Previously, we have developed a triblock copolymer system for generating low loss dielectric structures via direct-write 3D printing [2]. By incorporating ceramic nanoparticles into the polymer matrix, the dielectric constant of the printed material could be increased [3]. Our progress in expanding our materials palette of low loss dielectric inks as well as the integration of complex materials deposition approaches into our printing process is described below.

## II. MATERIALS AND CHARACTERIZATION

#### A. Composite Dielectrics

Our recent work has focused on increasing the dielectric constants of our inks while maintaining their low-loss characteristics. Our hypothesis was that by varying the ceramic nanoparticle content of our generated composite inks, we should be able to tune the dielectric constant of our printed structures. Hydrophobic styrene-isoprene-styrene (SIS) triblock polymers served as our model low dielectric polymer with a measured dielectric constant of 2.2 and loss tangent of 1.6 x 10<sup>-3</sup>. We selected TiO<sub>2</sub> and SrTiO<sub>3</sub> nanoparticles due to their high dielectric constants and low loss tangents. The surfaces of

Sebastien G. M. Uzel, Robert Weeks, and Jennifer A. Lewis

John A. Paulson School of Engineering and Applied Sciences Harvard University

Cambridge, MA, USA suzel@g.harvard.edu, rweeks@g.harvard.edu, jalewis@seas.harvard.edu

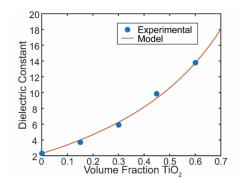


Fig. 1. Measured dielectric constant of TiO<sub>2</sub> composites

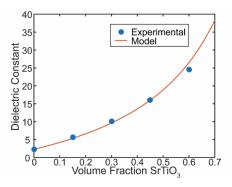


Fig. 2. Measured dielectric constants of SrTiO<sub>3</sub> composites

ceramic nanoparticles were functionalized to facilitate improved blending into the polymer matrix. Inks were formulated by combining the polymer and nanoparticles in volatile organic solvents and extruding the viscoelastic ink out of micron-sized nozzles. Structures with 0 % to 60 % volume fractions of ceramics were tested to determine their dielectric constants in the  $K_a$  band.

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The S-parameters from 26.5 to 40 GHz of a WR-28 waveguide loaded with composite were measured to calculate the dielectric constants and loss tangents with Keysight's proprietary software. These materials demonstrated median dielectric constants from 2-26.5 and loss tangents on the order of  $10^{-4} - 10^{-2}$  over the 26.5 to 40 GHz range as shown in Table I, Fig. 1, and Fig. 2. This behavior was dependent on the volume fraction of ceramic used and these results were modeled using effective medium theory [4] as:

$$\varepsilon = \varepsilon_{\rm B} \left[ 1 + \frac{f_{\rm A}(\varepsilon_{\rm A} - \varepsilon_{\rm B})}{\varepsilon_{\rm B} + n(1 - f_{\rm A})(\varepsilon_{\rm A} - \varepsilon_{\rm B})} \right] \tag{1}$$

where  $\epsilon$  is the effective permittivity of the composite,  $\epsilon_A$  is the permittivity of the particle,  $\epsilon_B$  is the permittivity of the polymer,  $f_a$  is the volumetric ratio of the particles within the polymer matrix, and n is the shape factor to account for particle morphology. From these data, we can predictively generate printable materials with a wide range of dielectric constants.

TABLE I. DIELECTRIC CHARACTERIZATION OF PRINTED COMPOSITES

Material (vol. %)	Dielectric Constant (ε') (34 GHz)	Loss Tangent (ε"/ε') (34 GHz)
SIS Polymer	2.2	0.002
TiO <sub>2</sub> /SIS (15:85)	3.7	0.005
TiO <sub>2</sub> /SIS (30 : 70)	5.9	0.012
TiO <sub>2</sub> /SIS (45 : 55)	9.9	0.016
TiO <sub>2</sub> /SIS (60 : 40)	13.8	0.028
SrTiO <sub>3</sub> /SIS (15 : 85)	5.6	0.035
SrTiO <sub>3</sub> /SIS (30 : 70)	10.1	0.032
SrTiO <sub>3</sub> /SIS (45 : 55)	16.0	0.033
SrTiO <sub>3</sub> /SIS (60 : 40)	24.6	0.050

# B. Conductive Composites

Our polymer-based system has also demonstrated compatibility with metallic particles. By incorporating metal flakes into our inks we are able to print conductive structures. As shown in Fig. 3, self-supporting metal composite traces of 200 µm can be effectively generated. The conductivities of printed traces were determined using a 4-wire resistance measurement. As shown in Table II we are able to generate metal composite structures that possess conductivities that are ~9 % of bulk silver. Notably, these results were obtained without the need for high temperature sintering conditions so as to maintain compatibility with the polymer dielectrics.

TABLE II. SUMMARY OF ELECTRICAL DATA FOR PRINTED WIRES

Material	Resistivity (Ω·m)	Conductivity (S/m)	% of Bulk Silver Conductivity
Bulk Silver	1.6 * 10-8	$6.3 * 10^7$	100
Commercial Silver Ink	7.4 * 10-6	1.4 * 105	0.2
Silver Flake Ink	1.8 * 10-7	5.7 * 10 <sup>6</sup>	9.1
Gold Flake Ink	8.3 * 10-7	1.2 * 106	1.9

## III. PRINTING METHODOLGY

To generate gradients of dielectrics, we have been developing a custom active mixing nozzle [5]. We are able to direct the dielectric constant of the final printed structure by



Fig. 3. Triangular lattice structure of printed silver composite

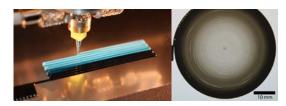


Fig. 4. Photograph of active mixing nozzle (left) and printed gradient

varying the polymer-to-nanoparticle ratio within the ink on-the-fly. Two syringe pumps, one filled with a high dielectric ink and the other with a low dielectric ink are combined within a mixing chamber prior to extrusion. Both the syringe pumps and nozzle are controlled using an Aerotech system. As shown in Fig. 4, the extruded filament can be programmably controlled eliminating the sharp transitions from individual inks and allowing for both geometric and compositional control over printed structures.

## IV. CONCLUSIONS

We have developed a series of conductive and dielectric inks for 3D printing RF devices. Combinations of the conductive and high dielectric constant materials allows the fabrication of complex structures that traditional manufacturing strategies cannot achieve. Furthermore, the ability to control the dielectric constant of a structure in a truly gradient fashion in 3 dimensions opens up a variety of novel architectures not previously realized.

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